LF to 4 GHz High Linearity Y-Mixer

Preliminary Technical Data

ADL5350

FEATURES

Broadband radio frequency (RF), intermediate frequency (IF), and local oscillator (LO) ports
Conversion loss: 6.8 dB
Noise figure: 6.5 dB
High input IP3: 25 dBm
High input P1dB: 19 dBm
Low LO drive level
Single-ended design: no need for baluns
Single-supply operation: 3 V @ 19 mA
Miniature 8-lead 3 mm x 2 mm LFCSP
RoHS compliant

APPLICATIONS

Cellular base station
Point-to-point radio links
RF instrumentation

FUNCTIONAL BLOCK DIAGRAM

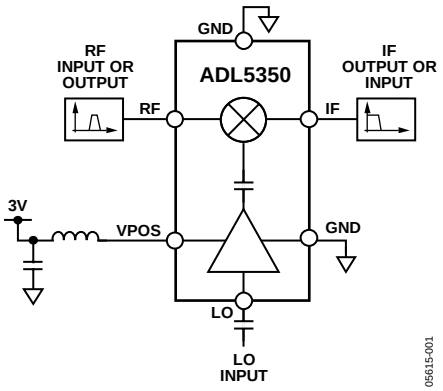

Figure 1.

GENERAL DESCRIPTION

The ADL5350 is a high linearity, up-and-down converting mixer capable of operating over a broad input frequency range. It is well suited for demanding cellular base-station mixer designs that require high sensitivity and effective blocker immunity. Based on a GaAs pHEMT, single-ended mixer architecture, the ADL5350 provides excellent input linearity and low noise figure without the need for a high power level local oscillator (LO) drive.

In 850 MHz/900 MHz receive applications, the ADL5350 provides a typical conversion loss of only 6.8 dB. The integrated LO amplifier allows a low LO drive level, typically only 4 dBm for most applications. The input IP3 is typically greater than 25 dBm, with an input compression point of 19 dBm. The high input linearity of the ADL5350 makes the device an excellent mixer for communications systems that require high blocker immunity, such as GSM 850/900 and 800 MHz CDMA2000. At 2 GHz, a slightly greater supply current is required to obtain similar performance.

The single-ended broadband RF/IF port allows the device to be customized for a desired band of operation using simple external filter networks. The LO to RF isolation is based on the LO rejection of the RF port filter network. Greater isolation may be achieved by using higher order filter networks, as described in the Applications Information section of this data sheet.

The ADL5350 is fabricated on a GaAs pHEMT, high performance IC process. The ADL5350 is available in a 3 mm x 2 mm 8-lead LFCSP. It operates over a −40°C to +85°C temperature range. An evaluation board is also available.

Rev. PrE

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SPECIFICATIONS

850 MHz RECEIVE PERFORMANCE

V_S = 3 V, T_A = 25°C, LO power = 4 dBm, re: 50 Ω, unless otherwise noted.

Table 1.

Parameter	Min	Typ	Max	Unit	Conditions
RF Frequency Range	750	850	975	MHz	
LO Frequency Range	500	780	945	MHz	Low-side LO
IF Frequency Range	30	70	250	MHz	
Conversion Loss		6.7		dB	f_{RF} = 850 MHz, f_{LO} = 780 MHz, f_{IF} = 70 MHz
SSB Noise Figure		6.4		dB	f_{RF} = 850 MHz, f_{LO} = 780 MHz, f_{IF} = 70 MHz
Input Third-Order Intercept		25		dBm	f_{RF1} = 849 MHz, f_{RF2} = 850 MHz, f_{LO} = 780 MHz, f_{IF} = 70 MHz; each RF tone 0 dBm
Input 1dB Compression Point		19.8		dBm	f_{RF} = 820 MHz, f_{LO} = 750 MHz, f_{IF} = 70 MHz
LO to IF Leakage		29		dBc	LO power = 4 dBm, f_{RF} = 850 MHz, f_{LO} = 780 MHz
LO to RF Leakage		13		dBc	LO power = 4 dBm, f_{RF} = 850 MHz, f_{LO} = 780 MHz
RF to IF Leakage		19.5		dBc	RF power = 0 dBm, f_{RF} = 850 MHz, f_{LO} = 780 MHz
IF/2 Spurious		–50		dBc	RF power = 0 dBm, f_{RF} = 850 MHz, f_{LO} = 780 MHz
Supply Voltage	2.7	3	3.5	V	
Supply Current		16.5		mA	LO power = 4 dBm

1950 MHz RECEIVE PERFORMANCE

V_S = 3 V, T_A = 25°C, LO power = 6 dBm, re: 50 Ω, unless otherwise noted.

Table 2.

Parameter	Min	Typ	Max	Unit	Conditions
RF Frequency Range	1800	1950	2050	MHz	
LO Frequency Range	1420	1760	2000	MHz	Low-side LO
IF Frequency Range	50	190	380	MHz	
Conversion Loss		6.8		dB	f_{RF} = 1950 MHz, f_{LO} = 1760 MHz, f_{IF} = 190 MHz
SSB Noise Figure		6.5		dB	f_{RF} = 1950 MHz, f_{LO} = 1760 MHz, f_{IF} = 190 MHz
Input Third-Order Intercept		25		dBm	f_{RF1} = 1949 MHz, f_{RF2} = 1951 MHz, f_{LO} = 1760 MHz, f_{IF} = 190 MHz; each RF tone 0 dBm
Input 1dB Compression Point		19		dBm	f_{RF} = 1950 MHz, f_{LO} = 1760 MHz, f_{IF} = 190 MHz
LO to IF Leakage		13.5		dBc	LO power = 6 dBm, f_{RF} = 1950 MHz, f_{LO} = 1760 MHz
LO to RF Leakage		10.5		dBc	LO power = 6 dBm, f_{RF} = 1950 MHz, f_{LO} = 1760 MHz
RF to IF Leakage		11.5		dBc	RF power = 0 dBm, f_{RF} = 1950 MHz, f_{LO} = 1760 MHz
IF/2 Spurious		–54		dBc	RF power = 0 dBm, f_{RF} = 1950 MHz, f_{LO} = 1760 MHz
Supply Voltage	2.7	3	3.5	V	
Supply Current		19		mA	LO power = 6 dBm

SPUR TABLES

All spur tables are $N \times f_{RF} - M \times f_{LO}$-mixer spurious products for 0 dBm input power, unless otherwise noted. N.M. indicates that a frequency was not measured. N.M. spurs are either less than −100 dBm or correspond to a frequency greater than 5995 MHz.

850 MHz SPUR TABLE

Table 3.

N \ M	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
0	N.M.	−22.8	−23.5	−18.7	−21.1	−40.5	−38.5	−27.8	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
1	−28.3	−6.3	−23.8	−19.6	−35.5	−24.4	−49.0	−38.3	−40.8	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
2	−46.3	−66.6	−46.8	−59.9	−50.3	−58.9	−51.1	−73.2	−61.2	−67.1	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
3	−73.8	−69.5	−79.2	−68.8	−84.7	−69.9	−72.8	−70.4	−88.6	−83.0	−81.6	N.M.	N.M.	N.M.	N.M.	N.M.
4	N.M.	−98.9	−96.7	N.M.	−93.4	N.M.	−92.7	−93.6	−91.0	N.M.	N.M.	N.M.	−91.5	N.M.	N.M.	N.M.
5	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
6	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
7	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
8	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
9	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
10	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
11	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
12	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
13	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
14	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
15	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.

1950 MHz SPUR TABLE

Table 4.

N \ M	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
0	N.M.	−11.7	−20.1	−28.5	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
1	−10.6	−7.1	−21.3	−25.3	−38.1	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
2	−48.3	−60.6	−44.0	−44.4	−49.0	−66.6	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
3	−77.4	−71.4	−86.9	−68.2	−66.0	−68.2	−79.9	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
4	N.M.	N.M.	−94.2	−92.0	−85.9	−82.9	−84.6	−90.1	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
5	N.M.	N.M.	N.M.	N.M.	−99.9	−95.4	−94.2	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
6	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
7	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
8	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
9	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
10	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
11	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
12	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
13	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
14	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.
15	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.	N.M.

ABSOLUTE MAXIMUM RATINGS

Table 5.

Parameter	Rating
Supply Voltage, V_S	4.0 V
RF Input Level	23 dBm
LO Input Level	20 dBm
Internal Power Dissipation	324 mW
θ_{JA}	154.3°C/W
Maximum Junction Temperature	135°C
Operating Temperature Range	−40°C to +85°C
Storage Temperature Range	−65°C to +150°C

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

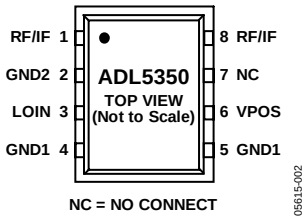

Figure 2. Pin Configuration

Table 6. Pin Function Descriptions

Pin Number	Mnemonic	Function
1, 8	RF/IF	RF and IF Input/Output Ports. These nodes are internally tied together. RF and IF port separation is achieved using external tuning networks.
2	GND2	Device Common (DC Ground) for RF/IF Switching Circuitry.
3	LOIN	LO Input, AC-Coupled.
4, 5	GND1	Device Common (DC Ground) for LO Buffer Circuitry.
6	VPOS	Positive Supply Voltage for the Drain of the LO Buffer. A series RF choke is needed on the supply line to provide proper ac loading of the LO buffer amplifier.
7	NC	No Connect.

TYPICAL PERFORMANCE CHARACTERISTICS

850 MHz CHARACTERISTICS

Supply voltage = 3 V, RF frequency = 850 MHz, IF frequency = 70 MHz, RF level = 0 dBm, LO level = 4 dBm, T_A= 25°C, unless otherwise noted.

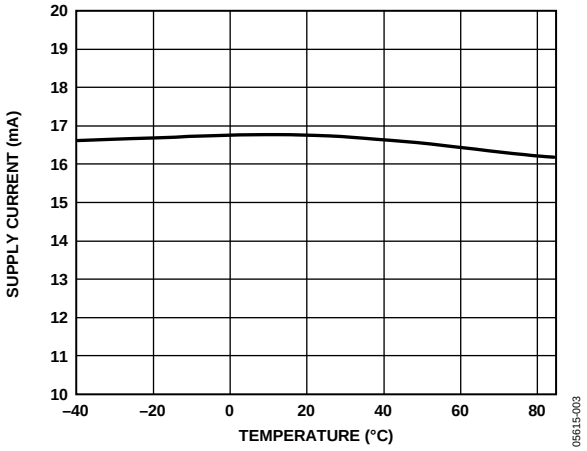

Figure 3. Current vs. Temperature

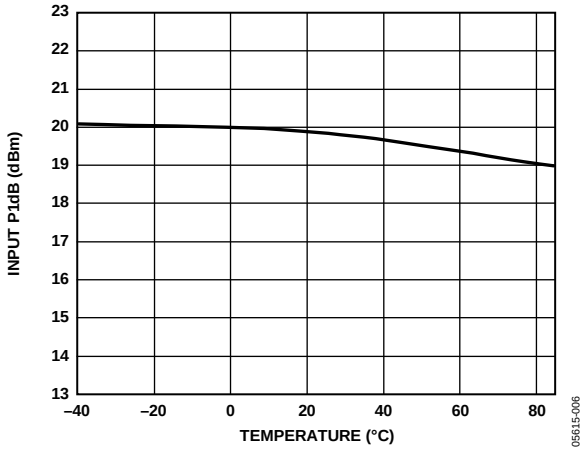

Figure 6. Input Compression vs. Temperature

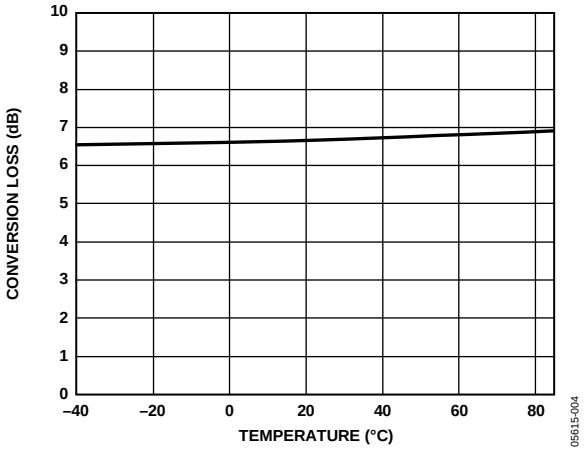

Figure 4. Conversion Loss vs. Temperature

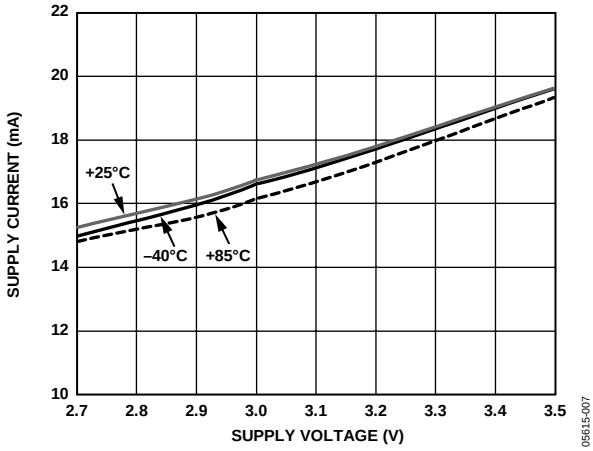

Figure 7. Current vs. Supply Voltage

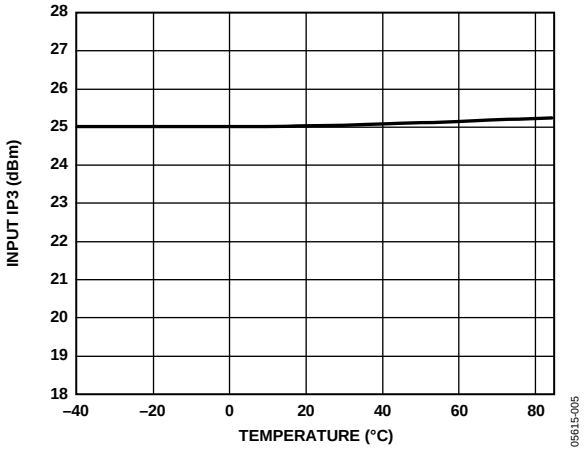

Figure 5. Input IP3(IIP3) vs. Temperature

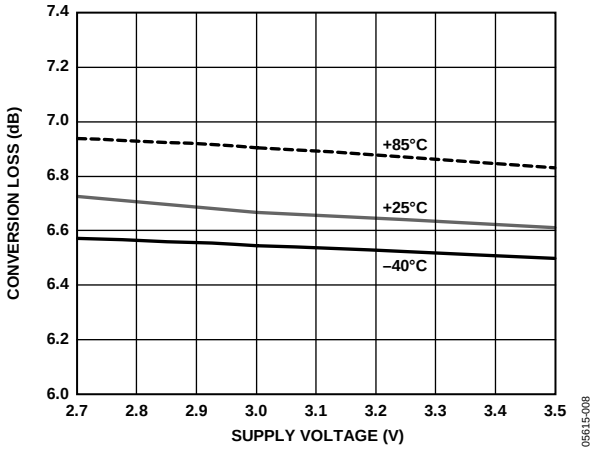

Figure 8. Conversion Loss vs. Supply Voltage

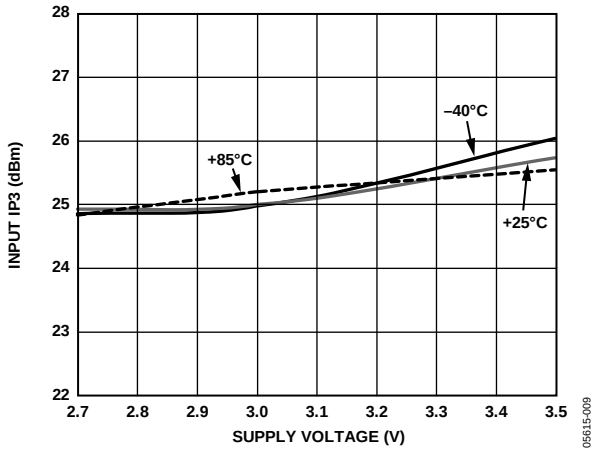

Figure 9. IIP3 vs. Supply Voltage

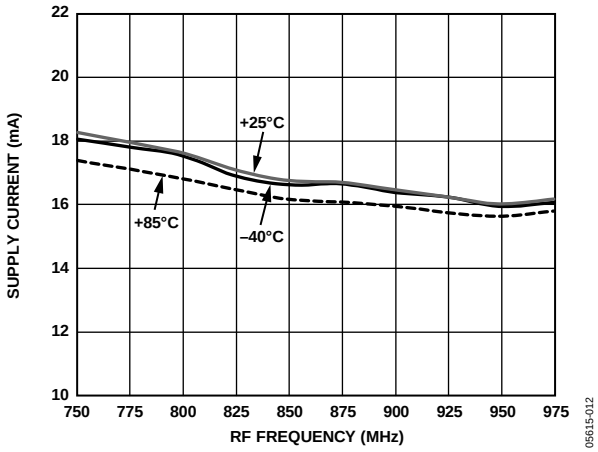

Figure 12. Current vs. RF Frequency

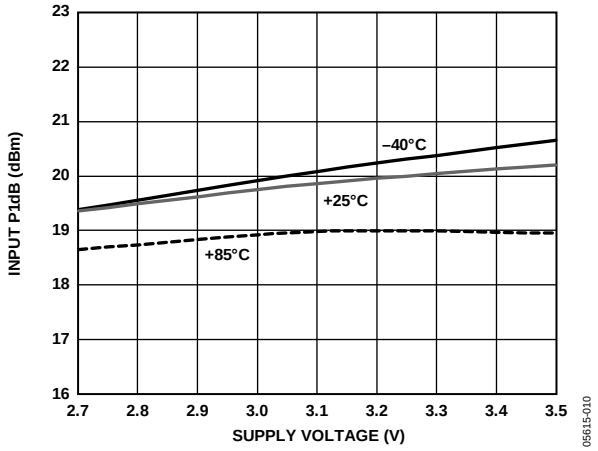

Figure 10. Input Compression vs. Supply Voltage

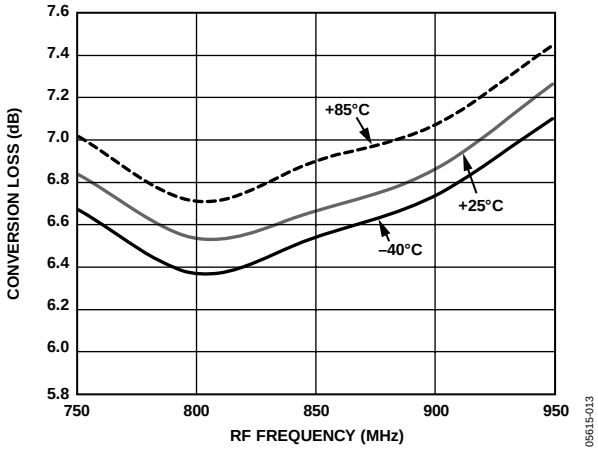

Figure 13. Conversion Loss vs. RF Frequency

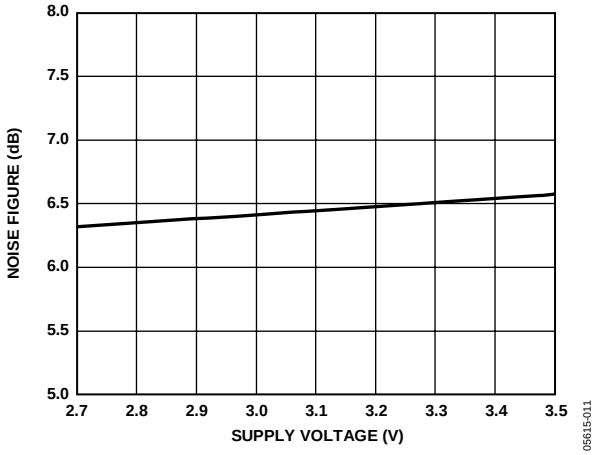

Figure 11. Noise Figure vs. Supply Voltage

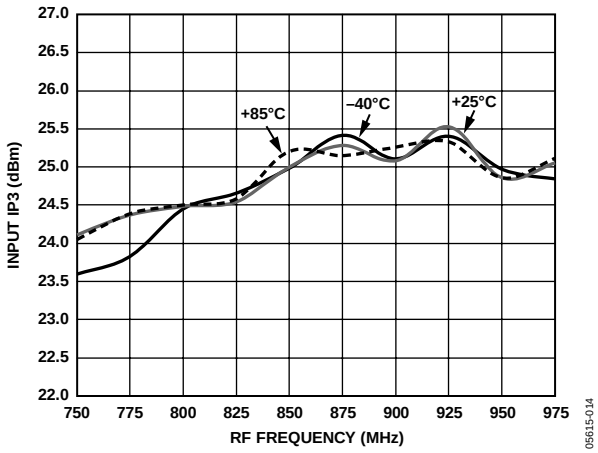

Figure 14. IIP3 vs. RF Frequency

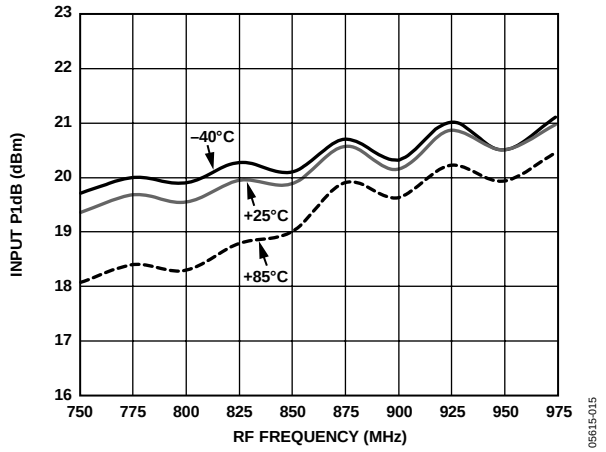

Figure 15. Input Compression vs. RF Frequency

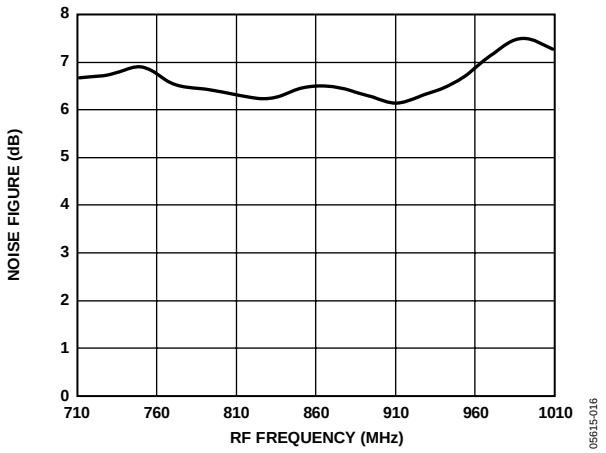

Figure 16. Noise Figure vs. RF Frequency

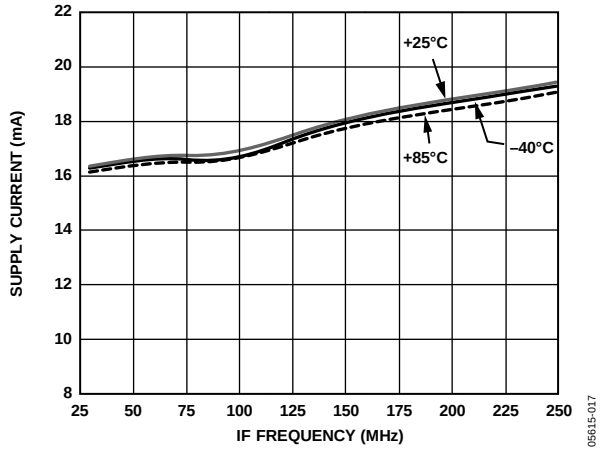

Figure 17. Current vs. IF Frequency

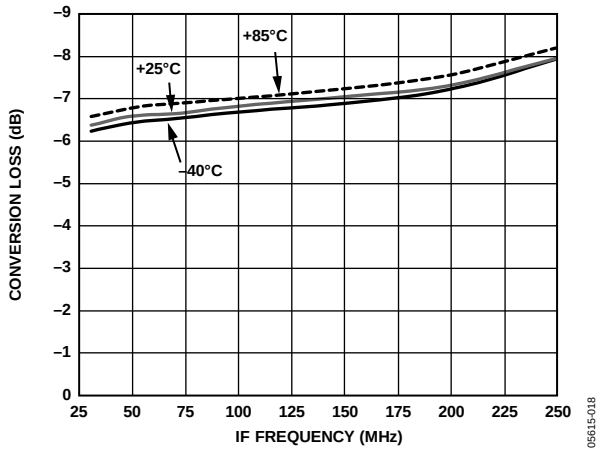

Figure 18. Conversion Loss vs. IF Frequency

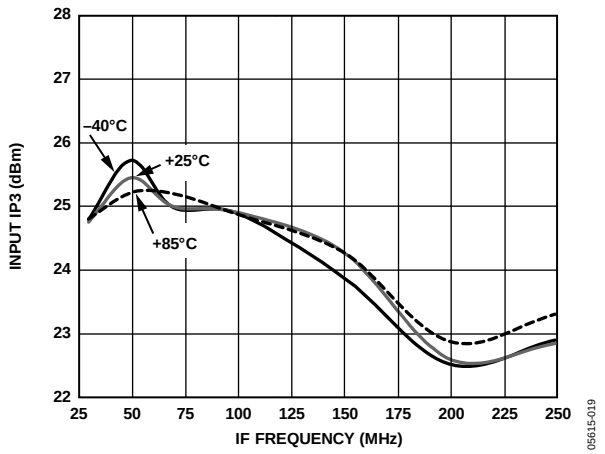

Figure 19. IIP3 vs. IF Frequency

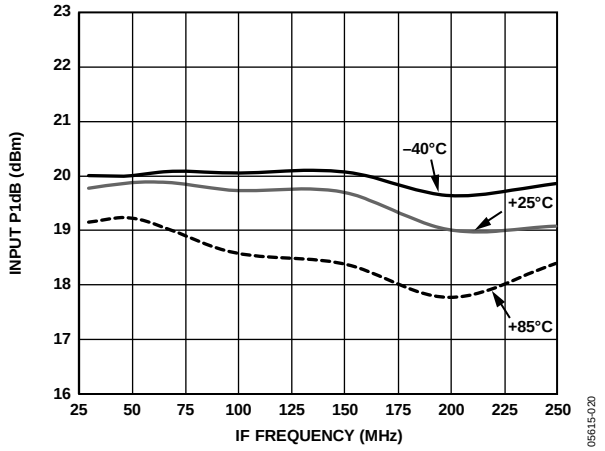

Figure 20. Input Compression vs. IF Frequency

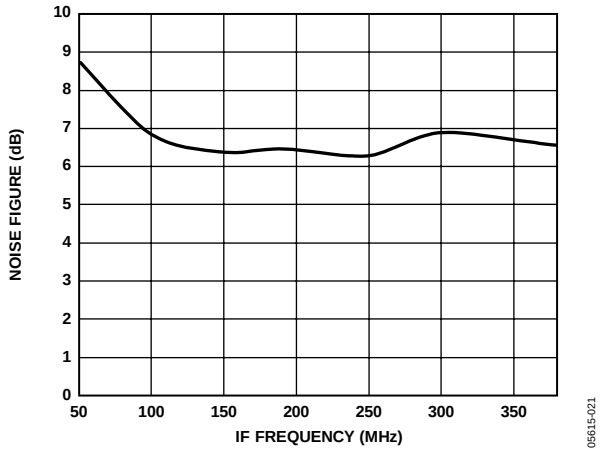

Figure 21. Noise Figure vs. IF Frequency

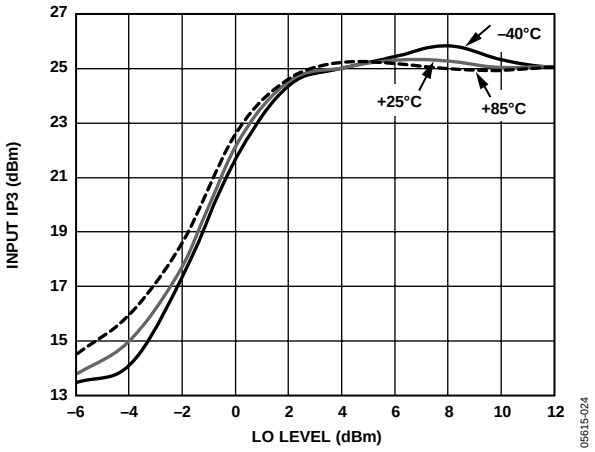

Figure 24. IIP3 vs. LO Level

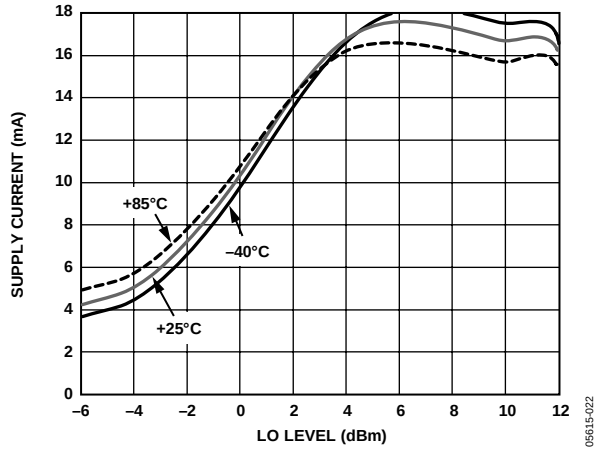

Figure 22. Current vs. LO Level

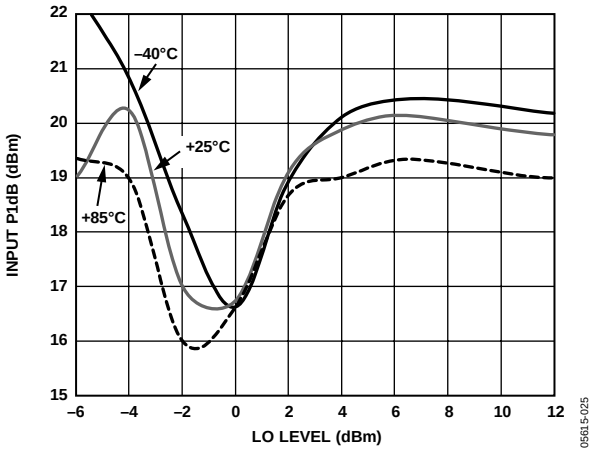

Figure 25. Input Compression vs. LO Level

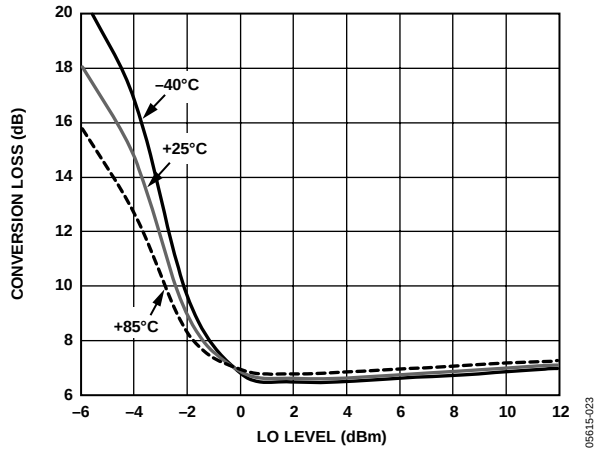

Figure 23. Conversion Loss vs. LO Level

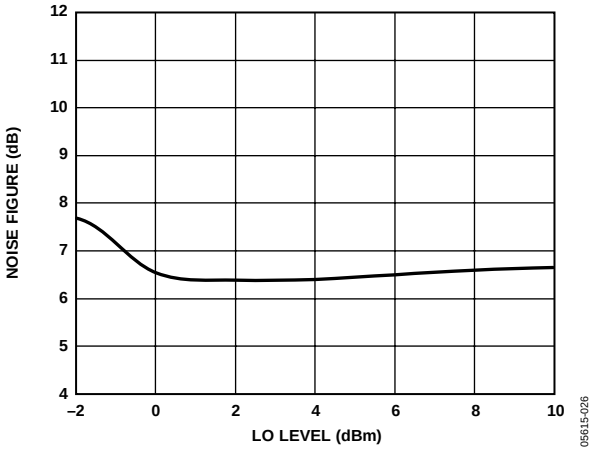

Figure 26. Noise Figure vs. LO Level

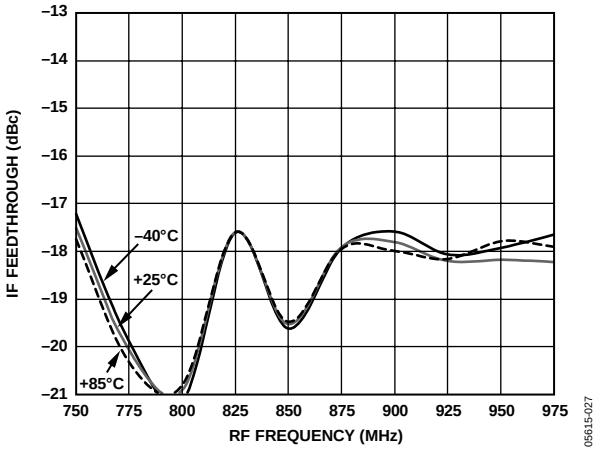

Figure 27. IF Feedthrough vs. RF Frequency

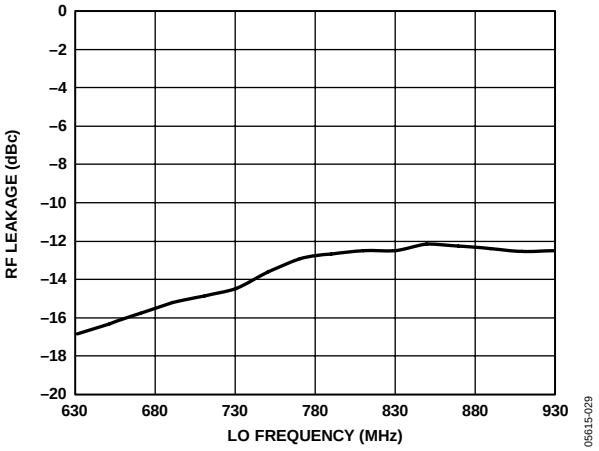

Figure 29. RF Leakage vs. LO Frequency

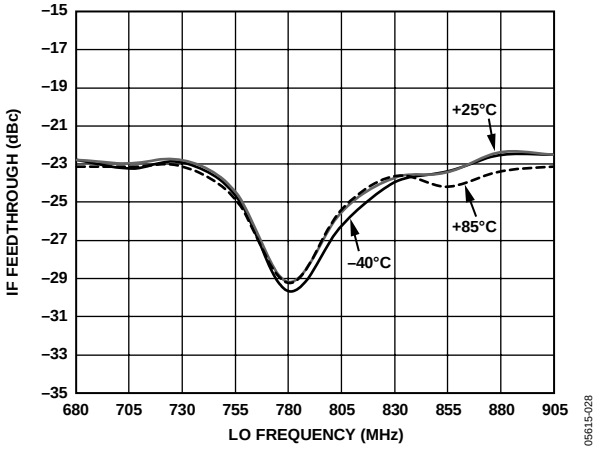

Figure 28. IF Feedthrough vs. LO Frequency

1950 MHz CHARACTERISTICS

Supply voltage = 3 V, RF frequency = 1950 MHz, IF frequency = 190 MHz, RF level = −10 dBm, LO level = 6 dBm, T_A = 25°C, unless otherwise noted.

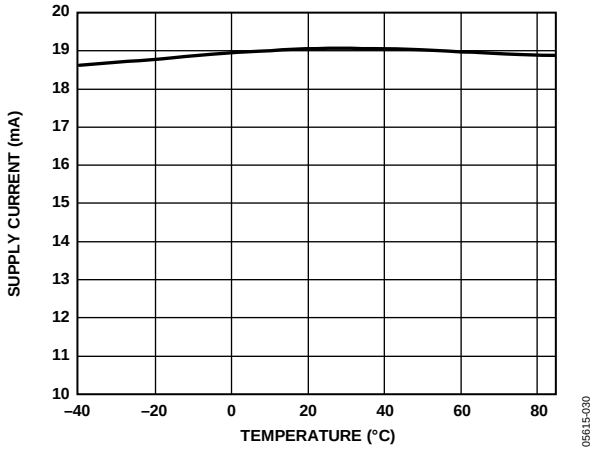

Figure 30. Current vs. Temperature

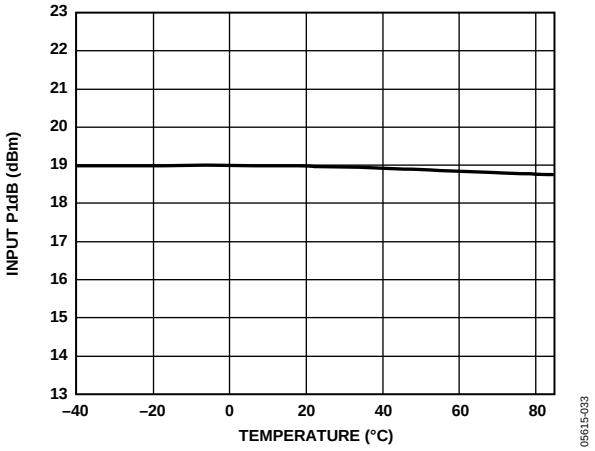

Figure 33. Input Compression vs. Temperature

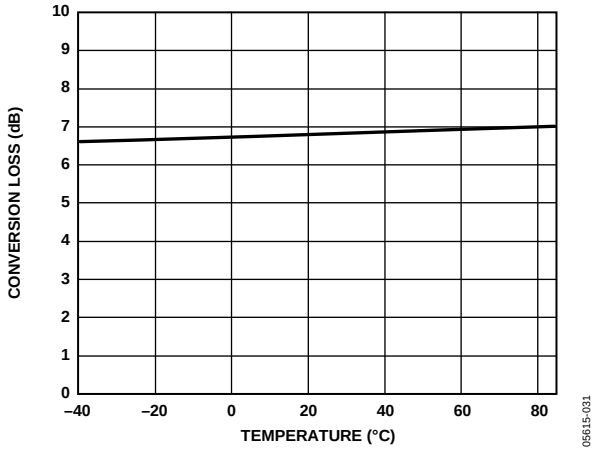

Figure 31. Conversion Loss vs. Temperature

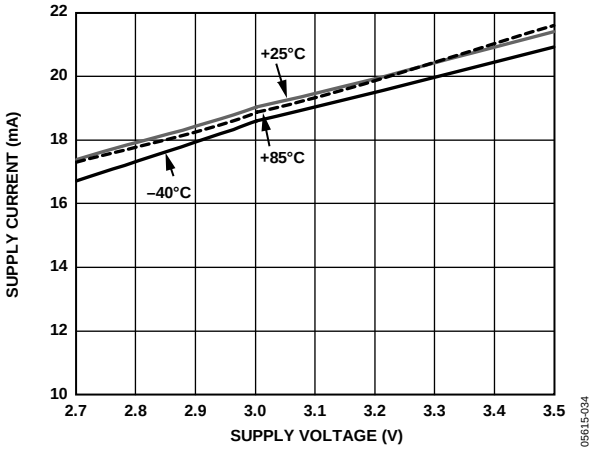

Figure 34. Current vs. Supply Voltage

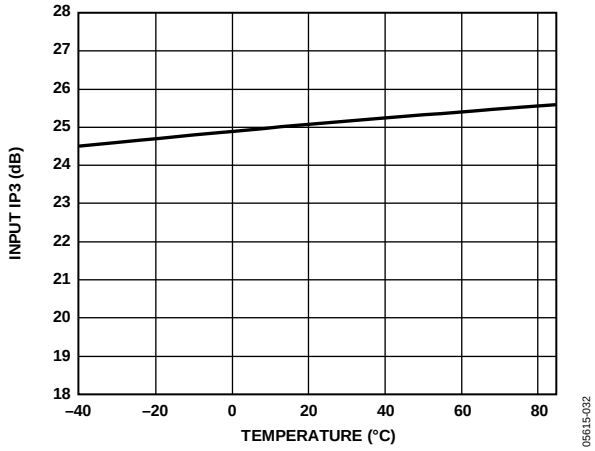

Figure 32. IIP3 vs. Temperature

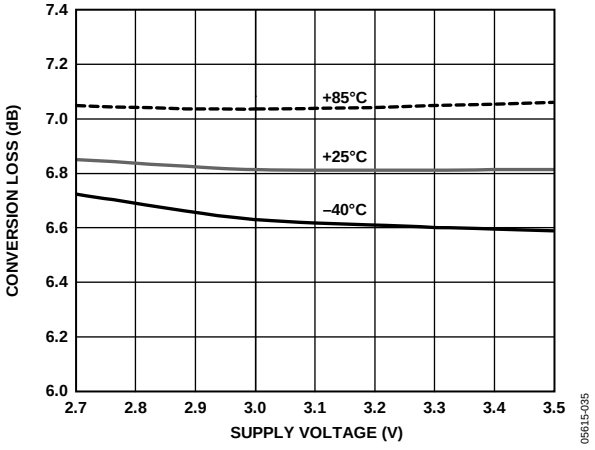

Figure 35. Conversion Loss vs. Supply Voltage

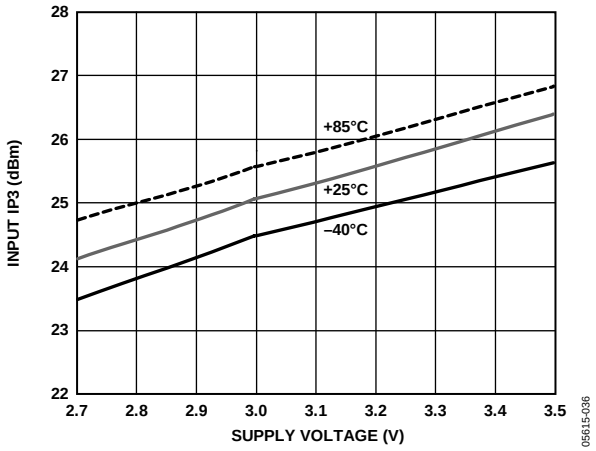

Figure 36. IIP3 vs. Supply Voltage

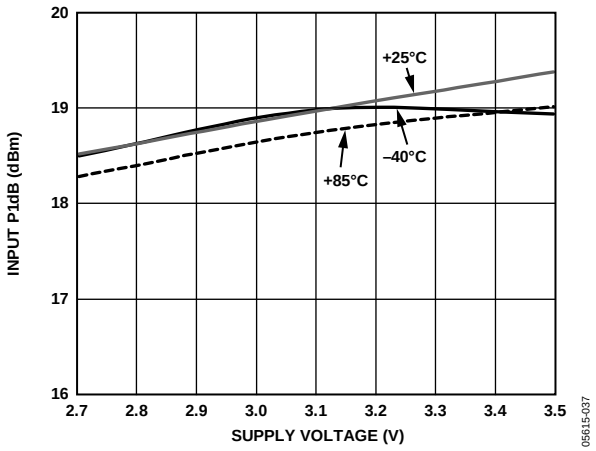

Figure 37. Input Compression vs. Supply Voltage

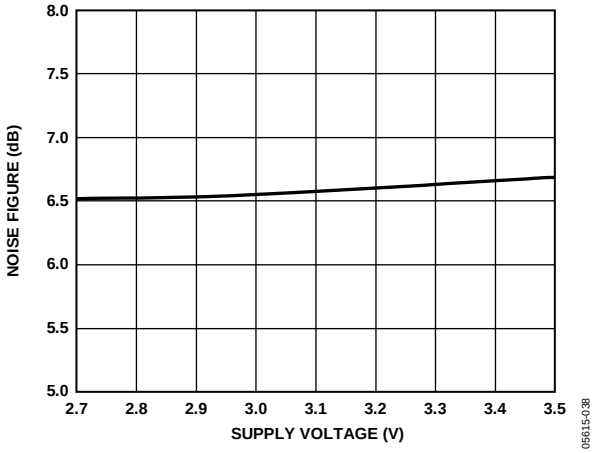

Figure 38. Noise Figure vs. Supply Voltage

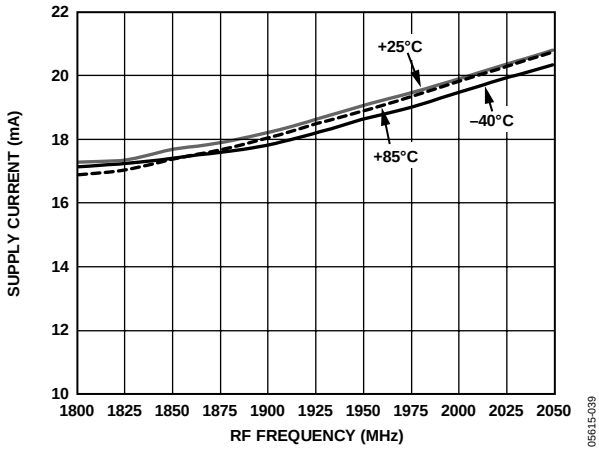

Figure 39. Current vs. RF Frequency

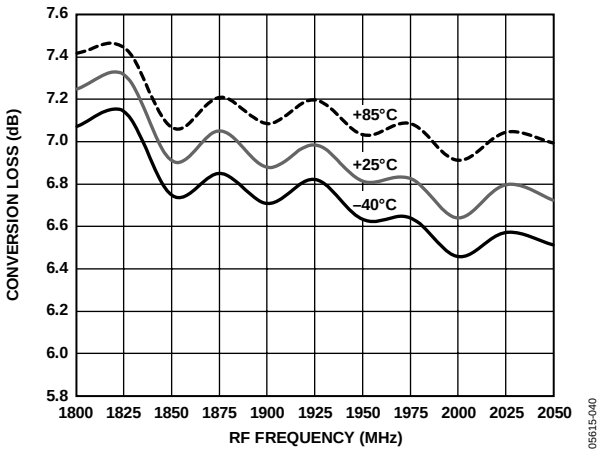

Figure 40. Conversion Loss vs. RF Frequency

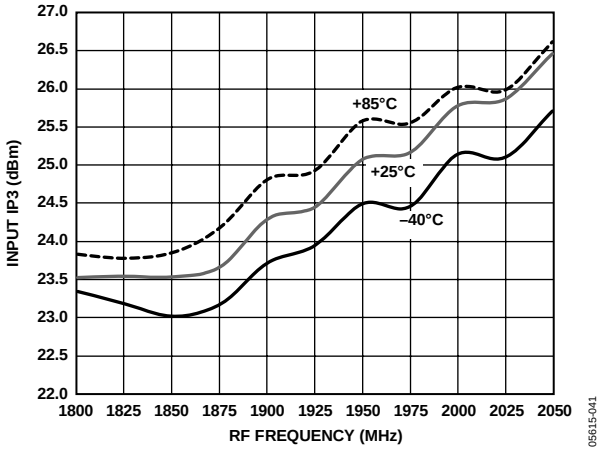

Figure 41. IIP3 vs. RF Frequency

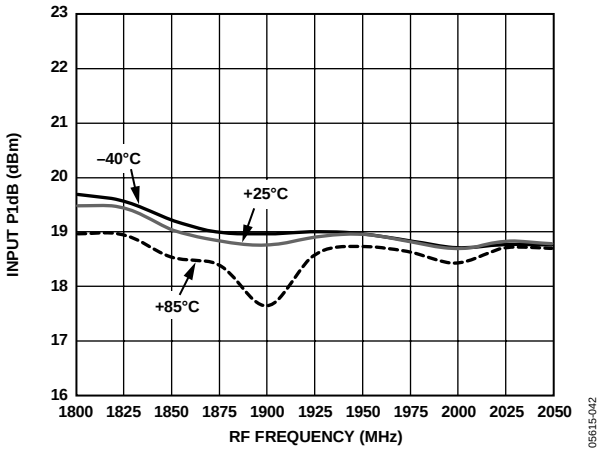

Figure 42. Input Compression vs. RF Frequency

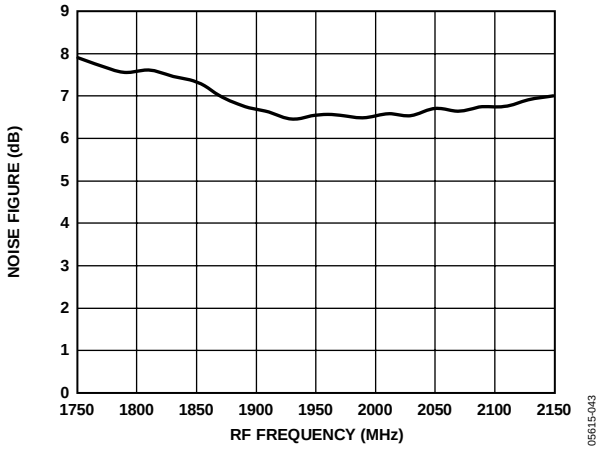

Figure 43. Noise Figure vs. RF Frequency

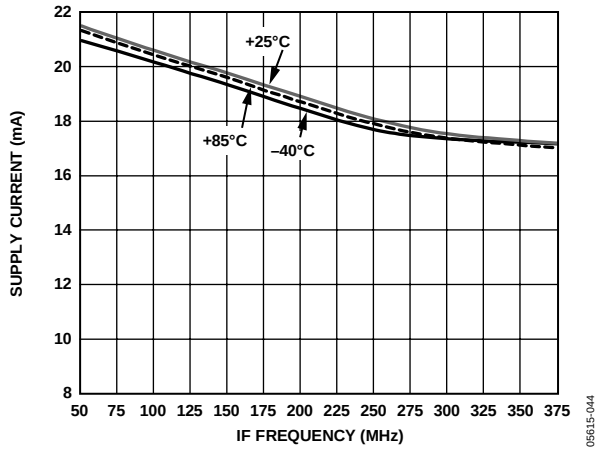

Figure 44. Current vs. IF Frequency

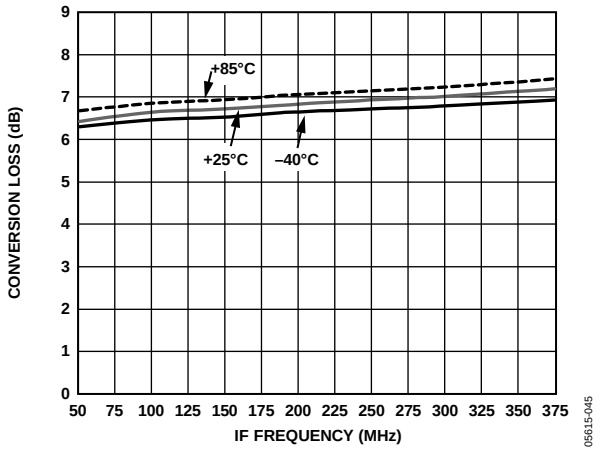

Figure 45. Conversion Loss vs. IF Frequency

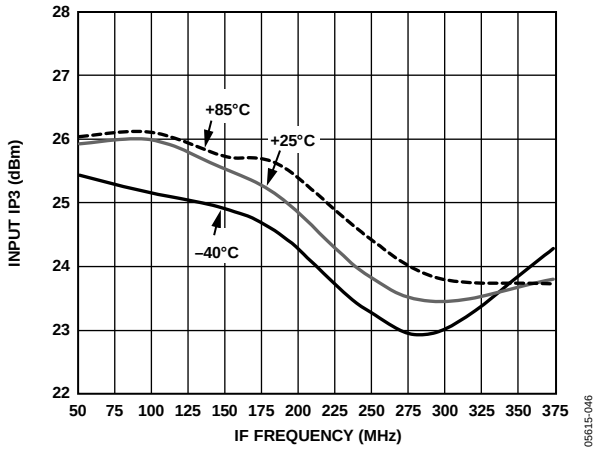

Figure 46. IIP3 vs. IF Frequency

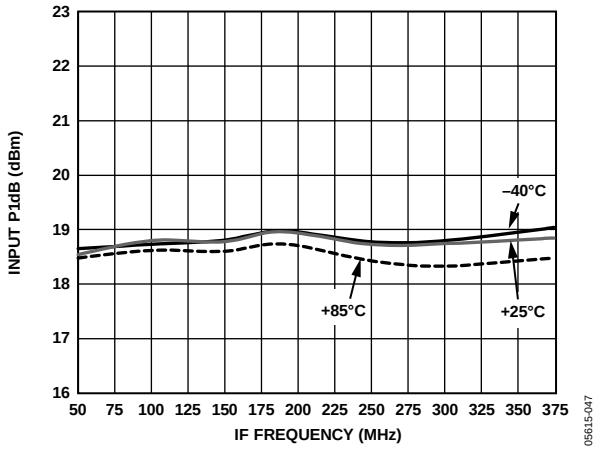

Figure 47. Input Compression vs. IF Frequency

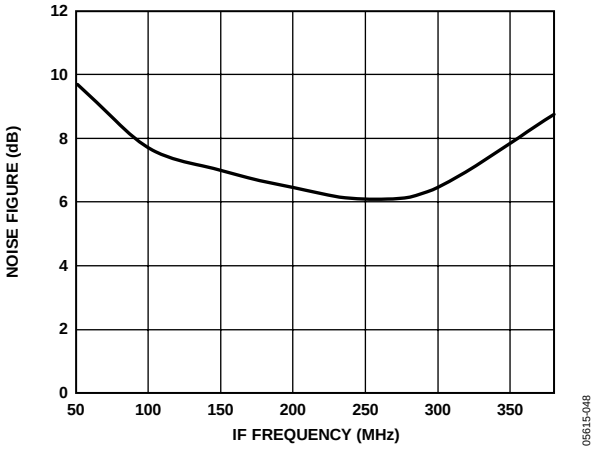

Figure 48. Noise Figure vs. IF Frequency

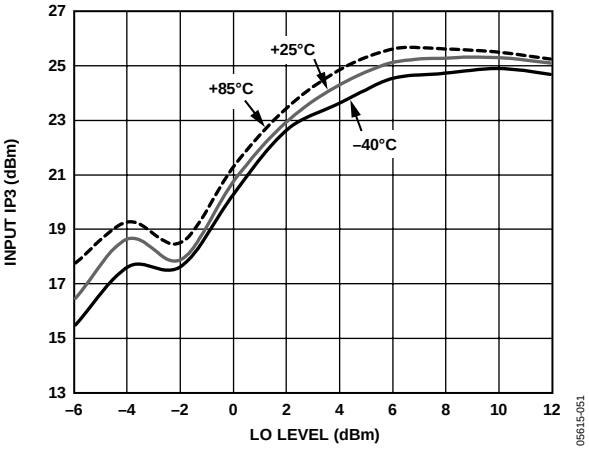

Figure 51. IIP3 vs. LO Level

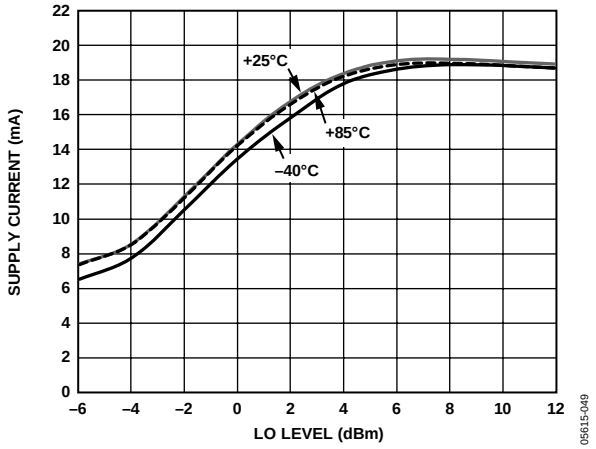

Figure 49. Current vs. LO Level

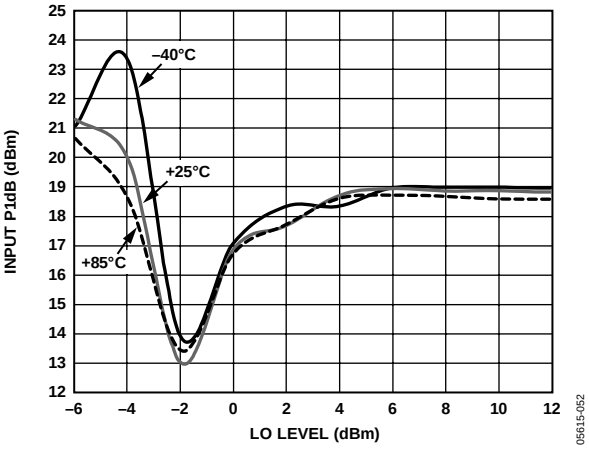

Figure 52. Input Compression vs. LO Level

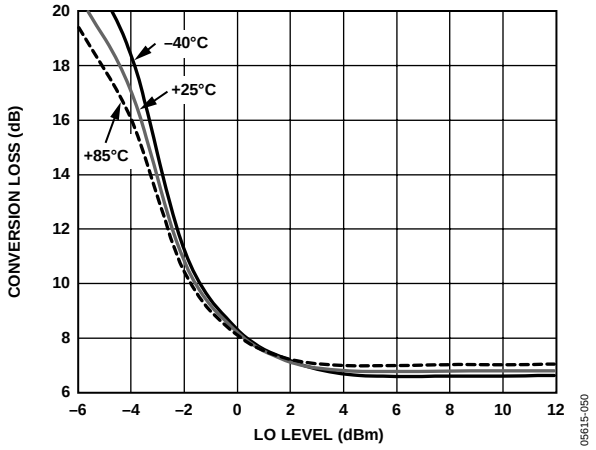

Figure 50. Conversion Loss vs. LO Level

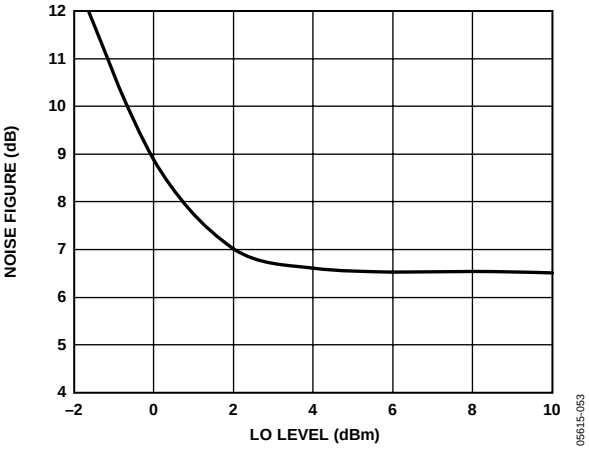

Figure 53. Noise Figure vs. LO Level

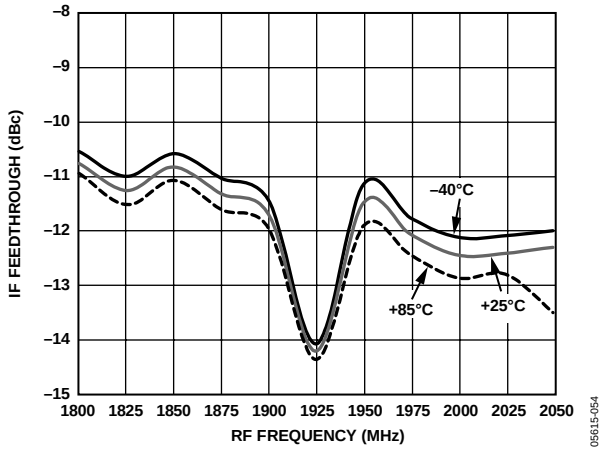

Figure 54. IF Feedthrough vs. RF Frequency

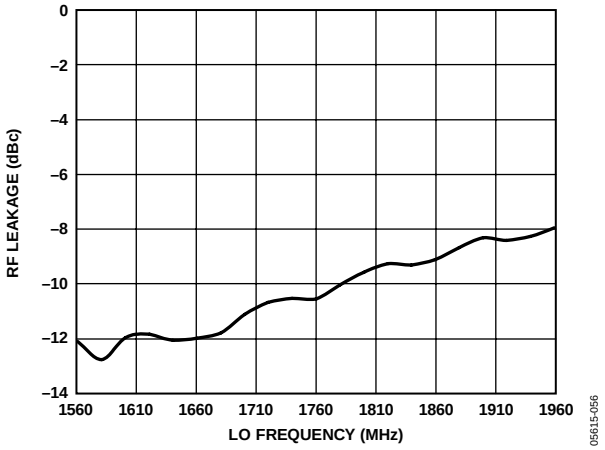

Figure 56. RF Leakage vs. LO Frequency

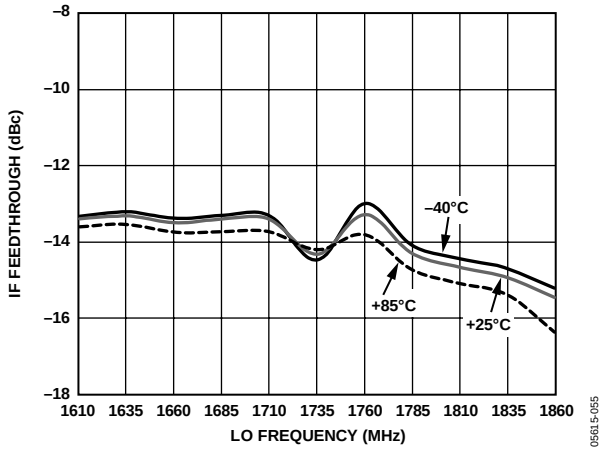

Figure 55. IF Feedthrough vs. LO Frequency

FUNCTIONAL DESCRIPTION

CIRCUIT DESCRIPTION

The ADL5350 is a GaAs pHEMT, single-ended, passive mixer with an integrated LO buffer amplifier. The device relies on the varying drain to source channel conductance of a FET junction to modulate an RF signal. A simplified schematic is shown in Figure 57.

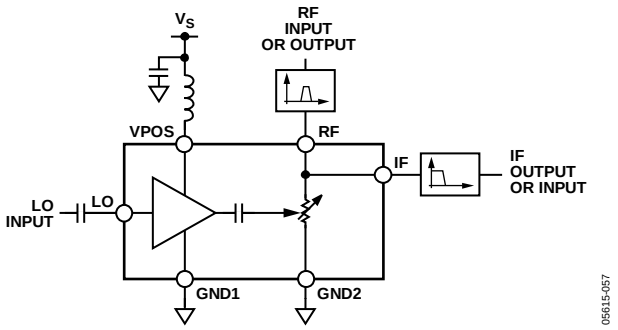

Figure 57. Simplified Schematic

The LO signal is applied to the gate contact of a FET-based buffer amplifier. The buffer amplifier provides sufficient gain of the LO signal to drive the resistive switch. Additionally, feedback circuitry provides the necessary bias to the FET buffer amplifier and RF/IF ports to achieve optimum modulation efficiency for common cellular frequencies.

The mixing of RF and LO signals is achieved by switching the channel conductance from the RF/IF port to ground at the rate of the LO. The RF signal is passed through an external band-pass network to help reject image bands and reduce the broadband noise presented to the mixer. The band-limited RF signal is presented to the time-varying load of the RF/IF port, which causes the envelope of the RF signal to be amplitude modulated at the rate of the LO. A filter network applied to the IF port is necessary to reject the RF signal and pass the wanted mixing product. In a downconversion application, the IF filter network is designed to pass the difference frequency and present an open circuit to the incident RF frequency. Similarly, for an upconversion application, the filter is designed to pass the sum frequency and reject the incident RF. As a result, the frequency response of the mixer is determined by the response characteristics of the external RF/IF filter networks.

IMPLEMENTATION PROCEDURE

The ADL5350 is a simple single-ended mixer that relies on off-chip circuitry to achieve effective RF dynamic performance. The following steps should be followed to achieve optimum performance (see Figure 58 for component designations):

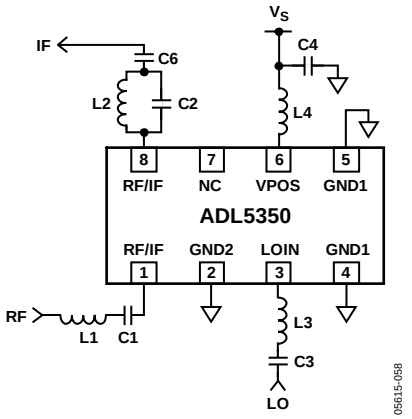

Figure 58. Reference Schematic

1. Tune LO buffer supply inductor for lowest supply current.

To start this procedure, it is necessary to provide an initial guess. Table 7 can be used as a starting point. It is not necessary to terminate or populate the RF and IF port networks to complete this first step. The RF/IF pins can be left open while tuning the LO buffer networks.

Table 7. Recommended LO Bias Inductor

Desired LO Frequency	Recommended LO Bias Inductor (L4)[1]
380 MHz	68 nH
750 MHz	24 nH
1000 MHz	18 nH
1750 MHz	3.8 nH
2000 MHz	2.1 nH

[1] The bias inductor should have a self-resonant frequency greater than the intended frequency of operation.

To test the supply current consumption, power up the device and apply the desired LO signal. Next, attempt to increase and decrease the LO frequency. If the current consumption increases as the LO frequency decreases, increase the value of L4. If the current consumption decreases as the LO frequency also decreases, decrease the value of L4. After determining the optimum inductor value, the current consumption should be minimized at the desired LO frequency.

2. Tune the LO port input network for optimum return loss.

Typically, a band-pass network is used to pass the LO signal to the LOIN pin. It is recommended to block high frequency harmonics of the LO from the mixer core. LO harmonics cause higher RF frequency images to be downconverted to the desired IF frequency and result in a sensitivity degradation. If the intended LO source has poor harmonic distortion and spectral purity, it may be necessary to employ a higher order band-pass filter network. Figure 58 illustrates a simple L-C band-pass filter used to pass the fundamental frequency of the LO source. Capacitor C3 is a simple DC block, while the series-inductor (L3), along with the gate-to-source capacitance of the buffer amplifier, form a low-pass network. The native gate input of the LO buffer (FET) alone presents a rather high input impedance. The gate bias is generated internally using feedback that can result in a positive return loss at the intended LO frequency. If a better than −10 dB return loss is desired, it may be necessary to add a shunt resistor to ground before the coupling capacitor (C3) to present a lower loading impedance to the LO source.

3. Design the RF and IF filter networks.

Figure 58 depicts simple LC tank filter networks for the IF and RF port interfaces. The RF port LC network is designed to pass the RF input signal. The series LC tank has a resonant frequency at $1/(2\pi\sqrt{LC})$. At resonance, the series reactances cancel, which presents a series short to the RF signal. A parallel LC tank is used on the IF port to reject the RF and LO signals. At resonance, the parallel LC tank presents an open circuit.

It is necessary to accommodate for the board parasitics, finite Q, and self-resonant frequencies of the LC components when designing the RF, IF, and LO filter networks. Table 8 provides suggested values for initial prototyping.

Table 8. Suggested RF, IF, and LO Filter Networks for Low-Side LO Injection

RF Frequency	L1[1]	C1	L2	C2	L3	C3
450 MHz	8.3 nH	10 pF	10 nH	10 pF	10 nH	100 pF
850 MHz	6.8 nH	4.7 pF	4.7 nH	5.6 pF	8.2 nH	100 pF
1950 MHz	1.7 nH	1.5 pF	1.7 nH	1.2 pF	3.5 nH	100 pF
2400 MHz	0.67 nH	1 pF	1.5 nH	0.7 pF	3.0 nH	100 pF

[1] The inductor should have a self-resonant frequency greater than the intended frequency of operation. L1 should be a high Q inductor for optimum NF performance.

APPLICATIONS INFORMATION

LOW FREQUENCY APPLICATIONS

The ADL5350 can be used in low frequency applications. The circuit in Figure 59 is designed for an RF of 136 MHz to 176 MHz and an IF of 45 MHz using a high-side LO. The series and parallel resonant circuits are tuned for 154 MHz, which is the geometric mean of the wanted RF frequencies. The performance of this circuit is depicted in Figure 60.

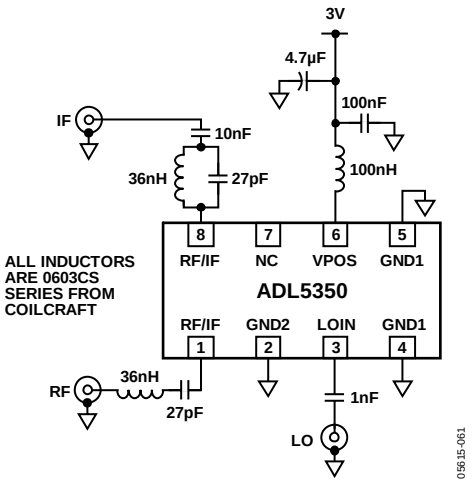

Figure 59. RF of 136 MHz to 176 MHz Downconversion Schematic

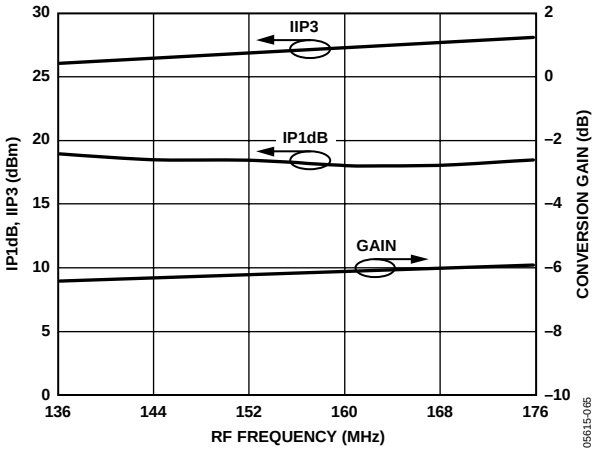

Figure 60. Measured Performance for Circuit in Figure 59 Using High-Side LO Injection and 45 MHz IF

HIGH FREQUENCY APPLICATIONS

The ADL5350 can be used at extended frequencies with some careful attention to board and component parasitics. Figure 61 is an example of a 2530 MHz to 2630 MHz down-conversion using a low-side LO. The performance of this circuit is depicted in Figure 62. Note that the inductor and capacitor values are very small, especially for the RF and IF ports. Above 2.5 GHz, it is necessary to consider alternate solutions to avoid unreasonably small inductor and capacitor values.

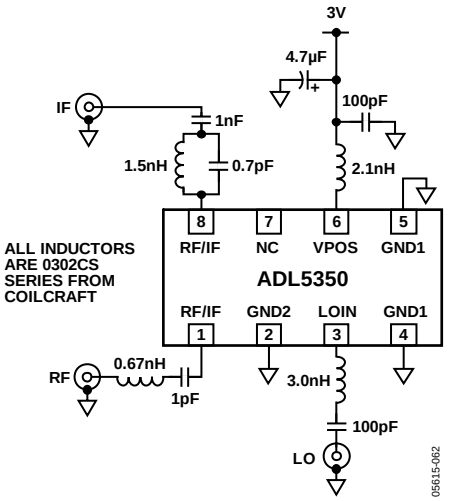

Figure 61. 2530 MHz to 2630 MHz RF Downconversion Schematic

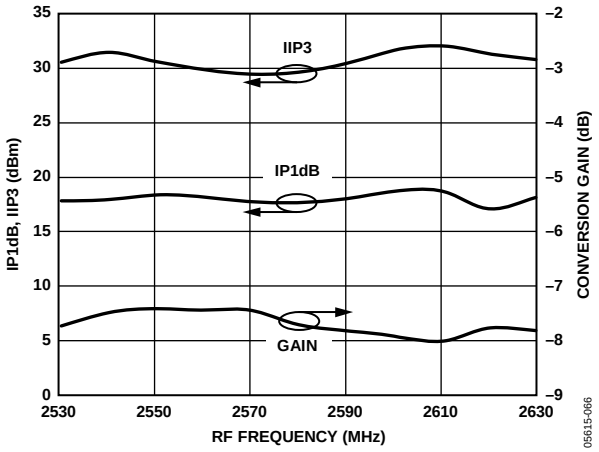

Figure 62. Measured Performance for Circuit in Figure 61 Using Low-Side LO Injection and 374 MHz IF

The typical networks used for cellular applications below 2.6 GHz utilize band-select and band-reject networks on the RF and IF ports. At higher RF frequencies, these networks are not easily realized by using lumped element components (discrete inductors and capacitors). As a result, it is necessary to consider alternate filter network topologies to allow more reasonable values of inductors and capacitors.

Figure 63 depicts a crossover filter network approach to provide isolation between the RF and IF ports for a downconverting application. The cross-over network essentially provides a high-pass filter to allow the RF signal to pass to the RF/IF node (Pin 1 and Pin 8), while presenting a low-pass filter (which is actually a band-pass filter when considering the DC blocking capacitor, C_{AC}). This allows the difference component ($f_{RF} - f_{LO}$) to be passed to the desired IF load.

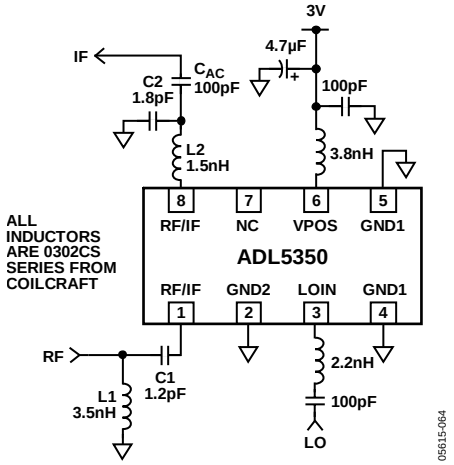

Figure 63. 3.3 GHz to 3.8 GHz RF Downconversion Schematic

When designing the RF port and IF port networks, it is important to remember that the networks share a common node (the RF/IF pins). In addition, the opposing network presents some loading impedance to the target network being designed.

Classic audio crossover filter design techniques can be applied to help derive component values. However, some caution must be applied when selecting component values. At high RF frequencies, the board parasitics can significantly influence the final optimum inductor and capacitor component selections. Some empirical testing may be necessary to optimize the RF and IF port filter networks. The performance of the circuit depicted in Figure 63 is provided in Figure 64.

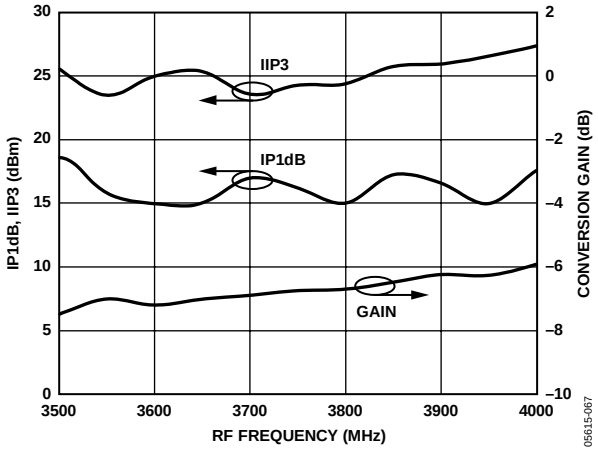

Figure 64. Measured Performance for Circuit in Figure 63 Using Low-Side LO Injection and 800 MHz IF

EVALUATION BOARD

An evaluation board is available for the ADL5350. The evaluation board has two halves: a low band board designated as Board A, and a high band board designated as Board B. The schematic for the evaluation board is presented in Figure 65.

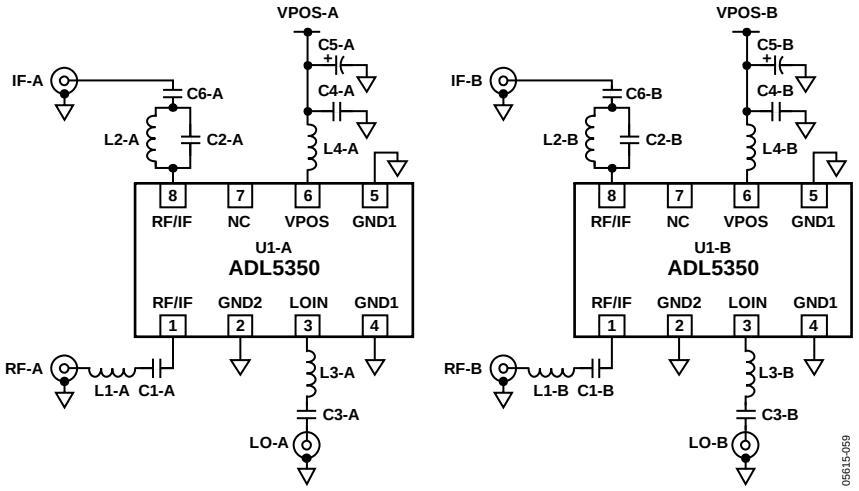

Figure 65. Evaluation Board

Table 9. Evaluation Board Configuration Options

Component	Function	Default Conditions
C4-A, C4-B, C5-A, C5-B	Supply Decoupling. C4-A and C4-B provide local bypassing of the supply. C5-A and C5-B are used to filter the ripple of a noisy supply line. These are not always necessary.	C4-A = C4-B = 100 pF, C5-A = C5-B = 4.7 µF
L1-A, L1-B, C1-A, C1-B	RF Input Network. Designed to provide series resonance at the intended RF frequency.	L1-A = 6.8 nH (0603CS from Coilcraft), L1-B = 1.7 nH (0302CS from Coilcraft), C1-A = 4.7 pF, C1-B = 1.5 pF
L2-A, L2-B, C2-A, C2-B, C6-A, C6-B	IF Output Network. Designed to provide parallel resonance at the geometric mean of the RF and LO frequencies.	L2-A = 4.7 nH (0603CS from Coilcraft), L2-B = 1.7 nH (0302CS from Coilcraft), C2-A = 5.6 pF, C2-B = 1.2 pF, C6-A = C6-B = 1 nF
L3-A, L3-B, C3-A, C3-B	LO Input Network. Designed to block DC and optimize LO voltage swing at LOIN.	L3-A = 8.2 nH (0603CS from Coilcraft), L3-B = 3.5 nH (0302CS from Coilcraft), C3-A = C3-B = 100 pF
L4-A, L4-B	LO Buffer Amplifier Choke. Provides bias and ac loading impedance to LO buffer amplifier.	L4-A = 24 nH (0603CS from Coilcraft), L4-B = 3.8 nH (0302CS from Coilcraft)

OUTLINE DIMENSIONS

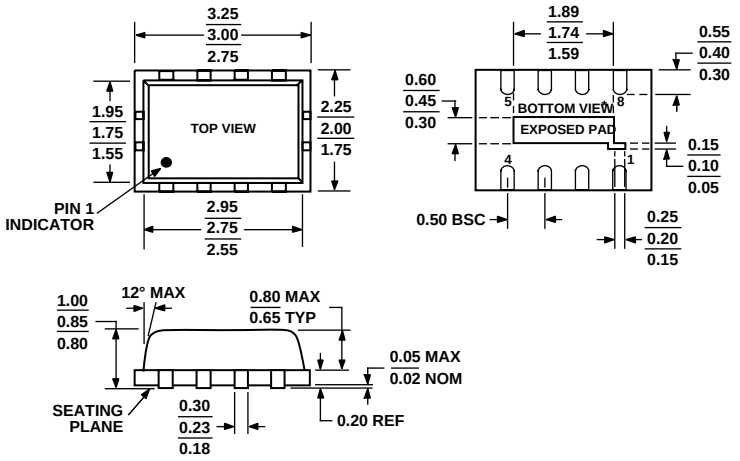

Figure 66. 8-Lead Lead Frame Chip Scale Package [LFCSP_VD]
2 mm × 3 mm Body, Very Thin, Dual Lead
(CP-8-1)
Dimensions shown in millimeters

ORDERING GUIDE

Model	Temperature Range	Package Description	Package Option	Branding	Ordering Quantity
ADL5350ACPZ-R2[1]	−40°C to +85°C	8-Lead Lead Frame Chip Scale Package [LFCSP_VD]	CP-8-1	Q7	250, Reel
ADL5350ACPZ-R7[1]	−40°C to +85°C	8-Lead Lead Frame Chip Scale Package [LFCSP_VD]	CP-8-1	Q7	3000, Reel
ADL5350ACPZ-WP[1]	−40°C to +85°C	8-Lead Lead Frame Chip Scale Package [LFCSP_VD]	CP-8-1	Q7	50, Waffle Pack
ADL5350-EVALZ[1]		Evaluation Board			

[1] Z = RoHS Compliant Part.

NOTES

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